

Saving Energy at WWTPs with the Bio-Tiger Model



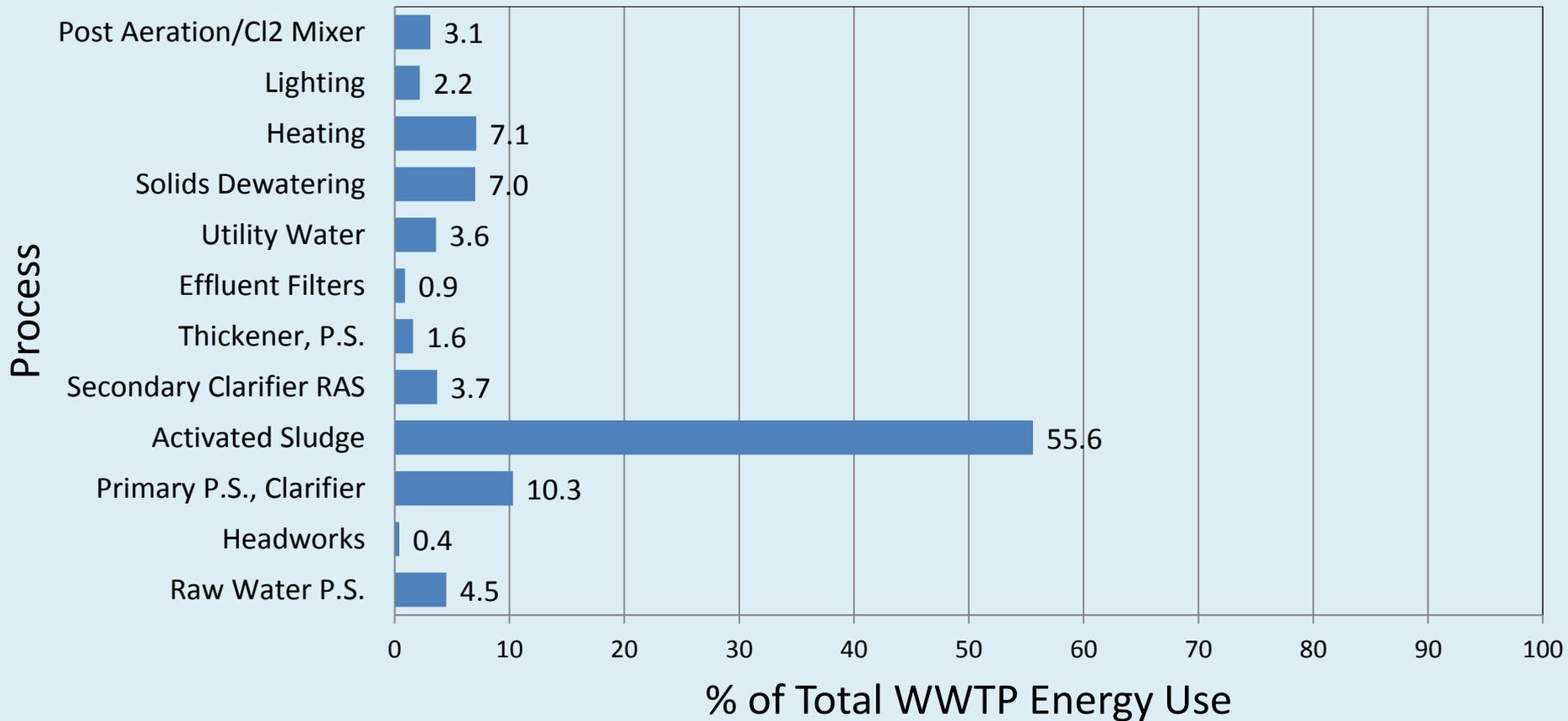
- Energy use for a given-size WWTP may vary significantly depending on:

- Location
- Strength of wastewater
- Level of treatment
- In-plant recovery
- Type of treatment process
- Mode of operation



- Relative distribution of energy use at a secondary wastewater treatment* plant:

Relative Distribution of Energy by Process



* Sample 7.5 MGD WWTP

- Energy costs account for:
 - 15 to 30% of the operation and maintenance (O&M) budgets at a large WWTP, and
 - 30 to 40% of O&M costs at a small WWTP.

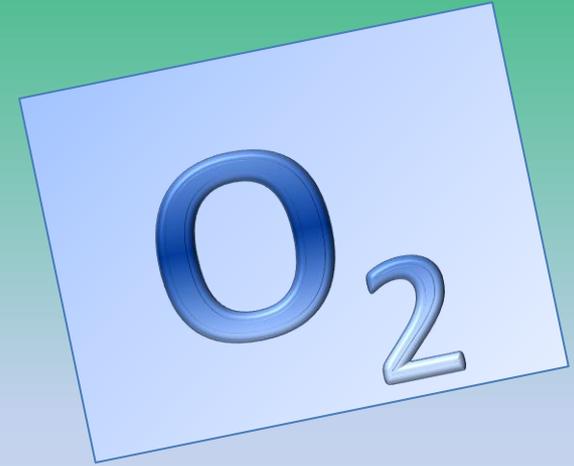


Secondary Treatment

- Overall, aeration devices used for the activated sludge system represent the most significant consumers of energy within a WWTP.
- Most aeration systems are classified as:
 - Diffused
 - Dispersed
 - Mechanical



- The ability of any type of equipment to dissolve oxygen within a wastewater treatment system depends on:
 - Diffuser device type
 - Basin geometry
 - Diffuser depth
 - Turbulence
 - Ambient air pressure
 - Temperature
 - Spacing and placement of the aeration devices
 - Diurnal variations in wastewater flow and organic load
 - **DO concentration in aerobic reactors**



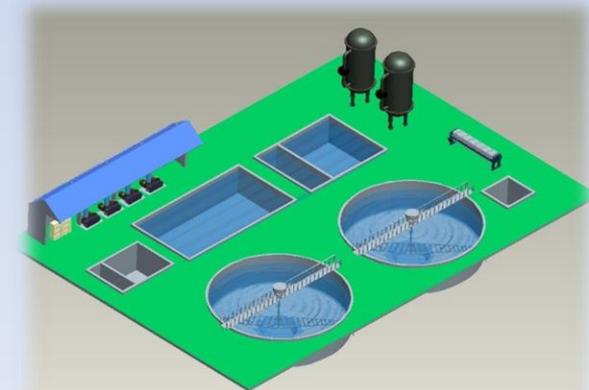
- Having high DO (dissolved oxygen) concentrations within aeration tanks is a waste of energy
- If the system uses blowers, an operator should cut back on blowers or blower output.
- If the facility has coarse bubble diffusers, then a fine-bubble-diffuser system that is more efficient and uses less energy should be considered.

- If a facility has surface aerators, the submergence on the unit may be decreased, which results in:
 - Less DO concentration
 - Less amperage load on the motor (less electrical cost)
- If the liquid level of the basin cannot be adjusted, then:
 - VFDs should be installed on the aerators, or
 - Aerators should automatically start and stop based on time intervals.

- Activated sludge aeration equipment uses large horsepower motors and multiple units such as:
 - Centrifugal-type blowers
 - Positive-displacement blowers
 - High-speed turbine (HST) blowers
 - Surface aerators
- Adding excessive air into the aeration tanks will only result in a waste of energy.

Questions?

- Improving the operation of aeration systems is one of the best ways to reduce the energy costs for wastewater treatment.
- The amount of oxygen required by the activated sludge process depends on:
 - Flow rate
 - Organic waste load
 - Oxidizable N load
 - SRT



- DO probes (sensors), in conjunction with online instrumentation systems perform the critical function of measuring DO levels in the aeration process.
- Typically, oxygen requirements vary throughout the day by a factor of 5 to 7 and can be regulated by automatically controlling systems.



- Air flowrates may be automatically adjusted by:
 - Changing blower speed
 - Adjusting blower inlet guide vanes
 - Operating control vanes
- A key to controlling the activated sludge process (and energy use) is matching oxygen supply to oxygen demand **while maintaining a reasonable DO concentration.**

- Typically, as wastewater flow and oxygen demand increase in the morning based on the diurnal flow of a WWTP, more aeration is needed.
- Conversely, as flow decreases during the night, the air supply should be reduced.



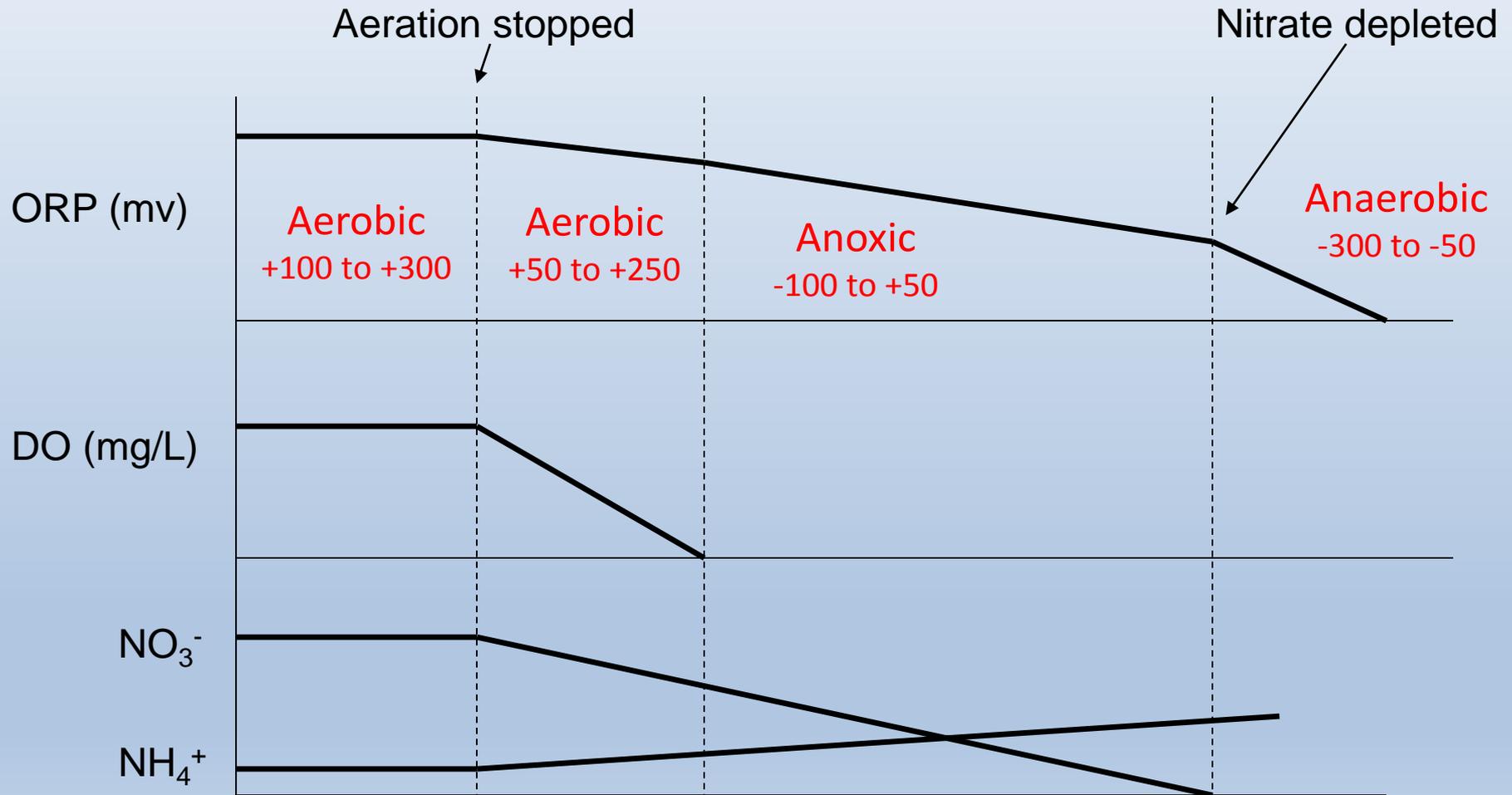
- A general rule has always been to maintain a DO concentration of 2mg/L in the aeration tanks.
- Once the carbonaceous and nitrogenous oxygen demand have been satisfied, maintaining any DO above 2 mg/L is excessive and a waste of energy.
- A number of treatment facilities maintain a DO concentration of 0.5 to 2.0 mg/L at the end of the aeration basin.

- Fine-bubble diffusers provide higher oxygen-transfer efficiencies as opposed to coarse-bubble diffusers.
- Installing fine-bubble diffusers into aeration basins will reduce the blower capacity needed to satisfy the process air demand.
- Less blower capacity will result in energy savings.

Intermittent Aeration for Energy Conservation in Oxidation Ditch

- Cycle time for on/off operation of aerators may vary
- Process control with DO and ORP monitoring
- When aerator is off, mixing is preferred
- During off period, oxidation ditch becomes anoxic reactor, and nitrate is consumed as bacteria degrade BOD
- ORP data are used to terminate off cycle and start aeration

Change in ORP and DO in On/Off Operation



Factors Affecting On/Off Operation

- Oxidation ditch HRT
- Influent flow rate
- TKN and BOD concentrations
- Number of on/off cycles per day
- Ditch MLSS concentration

Questions?

Bio-Tiger Model Training
March 4, 2021

Introduction to the Bio-Tiger Model

Providing Input Data to the Bio-Tiger Model for “Current Conditions”

Activated Sludge Input Data

Temperature (°C)	20
S_o - Influent BOD ₅ conc (mg/L)	200
V – volume of reactor (mil gal)	1
Q – influent flow rate (mgd)	1
Inert VSS (mg/L)	40
Oxidizable N (mg/L)	35
biomass (VSS/TSS)	0.85
Influent TSS (mg/L)	200
Inert Inorg TSS (mg/L)	20
Effluent TSS (mg/L)	8
RAS TSS (mg/L)	10000
MLSS (mg/L)	3000

f_d	0.1
Y	0.60
K_s (mg/L)	60
k_d at 20°C (1/day)	0.1
k at 20°C (1/day)	8

Aerator Performance Data	
Operating DO concentration (mg/L)	4.5
alpha	0.84
beta	0.92
SOTR, lb O ₂ / hp-hr	2.7
Temperature (°C)	20
Aeration (hp) being operated	150
Elevation (ft)	200
Aerators operating time (hr/day)	24
Type of aerators (1, 2, or 3)	1
Speed of aerators (%)	100
Energy cost unit (\$/kWh)	0.09

SRT (day)
1
2
4
6
8
10
12
14
16
18
20
22

Analysis

Revert to default

Reviewing Output Data from the Bio-Tiger Model for “Current Conditions”

Approximate Operating Conditions

Total average daily flow rate (mgd)	1.00
Aeration volume in service (mil gal)	1.00
Influent BOD5 concentration (mg/L)	200
Influent BOD5 mass loading (lb/day)	1,668
Sec ww Oxid N load (lb/day)	292
Sec ww TSS load (lb/day)	1,668
F/M ratio	0.089
Solids Retention Time (day)	28.0

MLSS (mg/L)	3,000
MLVSS (mg/L)	2,242
TSS Sludge Production (lb/day)	827
TSS in activated sludge effluent (lb/day)	66.7
Total Oxygen Requirements (lb/day)	3,121
Total Oxygen Req'd W/Denit. (lb/day)	2,687
Total oxygen supplied (lb/day)	3,394
Mixing intensity in the reactor (hp/mil gal)	150
RAS flow rate (mgd)	0.43
RAS recycle percentage (%)	42.9

WAS flow rate (mgd)	0.010
RAS TSS concentration (mg/L)	10,000
Total sludge production (lb/day)	894
Reactor Detention Time (hr)	24.0
VOLR (lb BOD/(thou cu ft-day))	12.48
Effluent CBOD5 (mg/L)	4.0
Effluent TSS (mg/L)	8.0
Effluent Ammonia-N (mg/L)	0.38
Effluent NO3-N (mg/L)	26.0
Effluent NO3-N W/denit (mg/L)	7.8

Actual Aerator Performance	
Field OTR (lb O2 / hp-hr)	0.94
Aerator energy use (kWh/month)	70,200
Energy cost (\$/month)	6,318

Questions?

Providing Input Data for an “Alternate Scenario”

Activated Sludge Input Data for Alternate Scenario

Temperature (°C)	20
S _o (mg/L)	200
V (mil gal)	1
Q (mgd)	1
Inert VSS (mg/L)	40
Oxidizable N (mg/L)	35
biomass (VSS/TSS)	0.85
Influent TSS (mg/L)	200
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f_d	0.1
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Analysis

Revert to default

Reviewing Output Data for an “Alternate Scenario”

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Actual Aerator Performance for "Alternate Scenario"	
Field OTR (lb O2 / hp-hr)	1.56
Aerator energy use (kWh/month)	39,780
Energy cost (\$/month)	3,580
Cost savings vs. current conditions (\$/month)	2,738

Questions?

Bio-Tiger Model Case Study

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